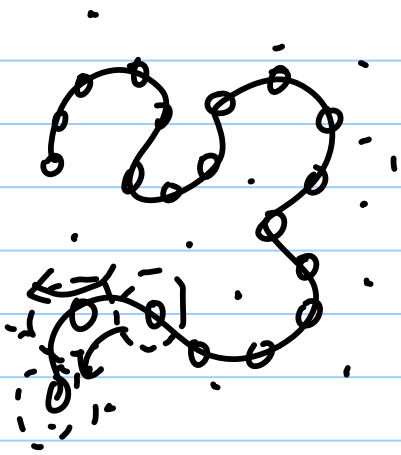


Dilute solns : polymer as ideal coil



- polymer thermal motion
- polymer solvent interaction
- solvent movement affect polymer motion
(hydrodynamic interaction)

treat polymer beads as Brownian particles

Exp't shows that the dynamics of polymers on scale $>$ blob size is generally independent of local monomer structure. (blob is the segment correlation length)

polymer \approx chain of blobs.

Solvent : consider as a continuum fluid

- exert fluctuating force & friction on polymer beads

EOM polymer : Langevin Equ. For the N polymer blobs

⇒ N - coupled EOM

Langevin Equ.

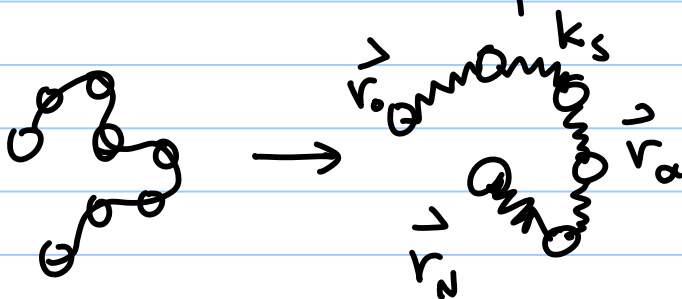
$$M \frac{d\vec{v}_\alpha}{dt} = \vec{F}_\alpha \quad \alpha = \text{particle } \alpha$$

↑ acceleration
↑ total force on α

Consider over damped in solvent
 polymer is purely diffusive: $\frac{d\vec{v}_\alpha}{dt} \rightarrow 0$

\vec{F}_α has multiple components.

(i) connectivity



$$U_{\text{intra polymer}}(\{\vec{r}_\alpha\}) = \frac{1}{2} k_s \sum_{\alpha=1}^{N-1} (\vec{r}_\alpha - \vec{r}_{\alpha+1})^2$$

$$+ \sum_{\alpha > \beta=1}^N U_{\text{exc. vol.}}$$

0 for ideal chains

$$\vec{F}_\alpha^{\text{intra}} = - \frac{\partial U}{\partial \vec{r}_\alpha}$$

linear Hooke's law

(2) local forces between polymer segments & solvent

$$\vec{F}_\alpha^{\text{fric}} = -\zeta \left(\vec{v}_\alpha - \vec{v}_{\text{fluid}}(\alpha) \right)$$
$$= -\zeta \vec{v}_\alpha$$

(3) Brownian fluctuations (thermal)

$\delta \vec{F}_\alpha(t)$ = fluctuating random force
on α (Gaussian)

$$\langle \delta \vec{F}_\alpha(t) \rangle = 0$$

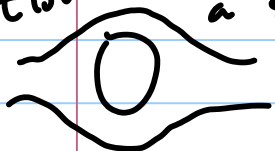
in one
coordinate

$$\langle \delta F_\alpha(t') \delta F_\beta(t'') \rangle = 2kT \zeta \delta_{\alpha\beta} \delta_{tt''}$$

"fluctuation - dissipation theorem".

$$\zeta = \text{friction coef. of blob} = 6\pi \eta_{\text{solvent}} \frac{b}{2}$$

flow around
a sphere



$b \equiv$ blob size

(Einstein - Stokes Relation)

$$D = \frac{kT}{\zeta}$$

Diffusivity
of a blob

(4) Hydrodynamic Interactions
purely solvent mediated force between
N-connected polymer segments



$\sim \frac{1}{r}$ Couple all segments

depends on the instantaneous configuration of polymer.

Generally, accounting all 4 effects are important. Very complex even for ideal coil

2 Classical models

I. Rouse model (1950s).

--- ignores hydrodynamics

assumes (i) ideal solvent

(ii) No HI

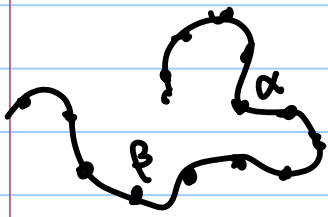
- turn out that (ii) is never valid for polymers in soln.

- Has several important physical aspects.

- Surprising good for dense polymer melts of "short, unentangled chains"

II Zimm model (1960s)

Rouse model + approx. inclusion of HI.

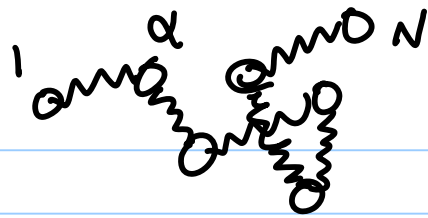


preaverages HI. $R_g \sim N^{1/2}$

$$V_\alpha(t) = H_{\alpha\beta}(t) V_\beta(t)$$

velocity of α preaveraged HI tensor

Rouse model



N segments \rightarrow N coupled EOM.

$$M \frac{d\vec{v}_\alpha}{dt} = \vec{F}_\alpha(t) \quad \alpha = 1..N$$

$\alpha = 2, 3, \dots, N-1$

$$0 = -k_s (2\vec{r}_\alpha - \vec{r}_{\alpha+1} - \vec{r}_{\alpha-1}) - \int \vec{v}_\alpha(t) + \delta \vec{F}_\alpha(t)$$

$\alpha = 1, N$

$$\begin{cases} 0 = -k_s (\vec{r}_1 - \vec{r}_2) - \int \vec{v}_1(t) + \delta \vec{F}_1(t) \\ 0 = -k_s (\vec{r}_{N-1} - \vec{r}_N) - \int \vec{v}_N(t) + \delta \vec{F}_N(t) \end{cases}$$

\Rightarrow a system of N linear coupled eqns w/
const. coeffs.

\rightarrow 1st order stochastic differential eqns.

N -coupled oscillators \Rightarrow Normal mode analysis

"Normal coordinates" "Phonons"

Collective quantities

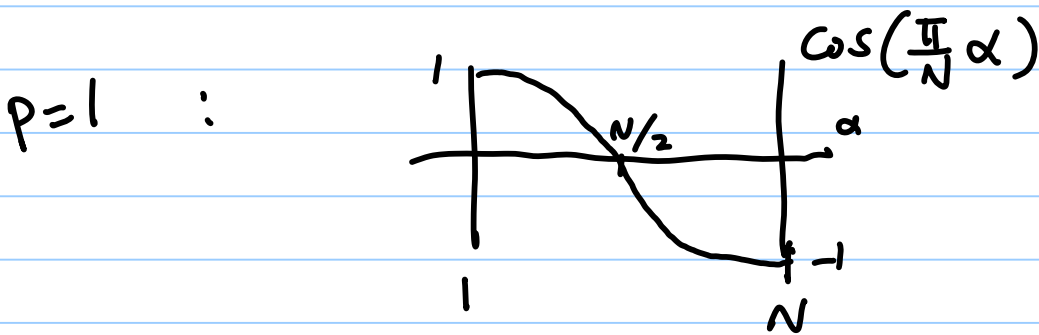
Dynamics of each mode is independent
(orthogonal)

mode $\left\{ \begin{array}{l} \vec{X}_p \equiv \frac{1}{N} \sum_{\alpha=1}^N \cos\left(\frac{p\pi\alpha}{N}\right) \vec{r}_\alpha(t) \\ \uparrow \\ \text{mode index} \\ p = 0, \dots, N-1 \end{array} \right.$ Cosine transform

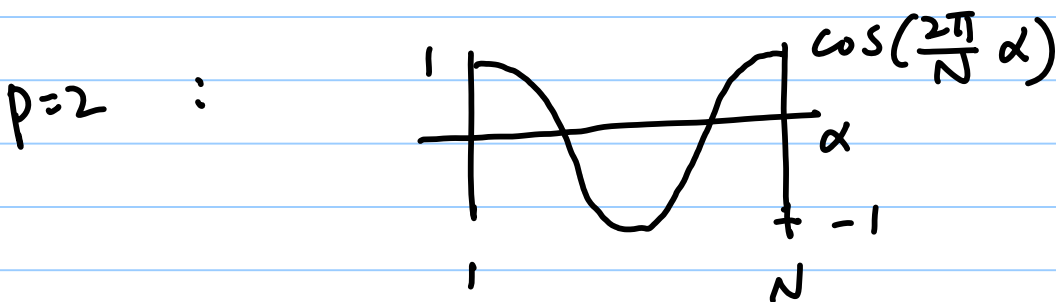
$\langle \vec{X}_p(t) \vec{X}_q(t) \rangle = 0 \quad \text{if } p \neq q.$

Rouse modes \approx "standing waves" along chain backbone

$p=0$: Center of mass motion



Sensitive to the orientation of whole polymer



divides chain into two halves & probe the orientation of 2 halves

As $p \uparrow$, modes further decompose chain into smaller units. Smallest unit = length of segment

Cosine transform can be inverted

$$\vec{x}_p = \frac{1}{N} \sum_{\alpha=1}^N \vec{r}_{\alpha}(t) \cos\left(\frac{p\pi}{N} \alpha\right)$$

$$\vec{r}_{\alpha} = \vec{x}_0(t) + 2 \sum_{p=1}^{N-1} \cos\left(\frac{p\pi}{N} \alpha\right) \vec{x}_p(t)$$

① Internal mode displacements

$$C_{pp'}(t) \equiv \langle \vec{x}_{p'}(0) \vec{x}_p(t) \rangle$$

Cosine transform of N -EOM

$$\text{Eqn. (1)} \quad \int_p \frac{\partial}{\partial t} \vec{x}_p(t) = -k_p \vec{x}_p(t) + \int \vec{f}_p(t)$$

$$\text{Eqn. (2)} \quad \int_p = \begin{cases} 2N \int & , p > 0 \\ N \int & , p = 0. \end{cases}$$

$$k_p = \text{spring const. of mode } p = 2\pi^2 k_s \frac{p^2}{N}$$

$$k_s = \frac{3kT}{b^2} \Rightarrow$$

$$k_p = \frac{6\pi^2}{Nb^2} kT p^2$$

$$C_{pp'}(t) = \delta_{p,p'} \frac{3k_B T}{k_p} e^{-t/\tau_p}$$

$$\tau_p \equiv \frac{\beta_p}{k_p} = \underbrace{\left(\frac{J N^2 b^2}{3\pi^2 k_B T} \right)}_{\text{Rouse relaxation time of mode } p} \frac{1}{p^2}$$

τ_R = longest relaxation time of internal modes.

$$(i) \tau_R \propto \frac{N^2 J}{T}$$

(ii) $\tau_p \propto \frac{1}{p^2} \Rightarrow$ faster relaxation as cooperative length scale decreases.

② Center-of-mass motion

$$\vec{x}_{p=0}(t) = \frac{1}{N} \sum_{\alpha=1}^N \vec{r}_{\alpha}(t).$$

Sub. into Equ. (1)

$$\langle \vec{x}_0(t) \vec{x}_0(0) \rangle = \langle \vec{x}_0^2 \rangle e^{-t/\tau_p} \Big|_{p=0}.$$

$$\langle \vec{x}_0^2 \rangle = \frac{3k_B T}{k_p} \rightarrow \infty \text{ as } p \rightarrow 0.$$

COM diffusion is unbounded over macroscopic distances $\tau_p \rightarrow \infty$ as $p \rightarrow 0$

$$\langle (\vec{x}_0(t) - \vec{x}_0(0))^2 \rangle$$

$$= 2 \left[\langle \vec{x}_0(0) \rangle^2 - \langle \vec{x}_0(0) \cdot \vec{x}_0(t) \rangle \right]$$

$$= 2 \langle \vec{x}_0(0) \rangle^2 \left[1 - e^{-t/\tau_p} \right]_{p \rightarrow 0}$$

$\rightarrow \infty$ $\rightarrow 0$

Equ. 2.

$$\rightarrow = \frac{6k_B T t}{\zeta_p = 0} = \frac{6k_B T t}{N \zeta_0}$$

\leftarrow friction of a segment.

CoM diffusion coef.

$$\langle \Delta r^2 \rangle = 6 D t$$

$$D_{\text{CoM}} = \frac{k_B T}{N \zeta_0}$$

\leftarrow friction of polymer

$$\zeta_{\text{polymer}} = N \zeta_0$$

total friction on a polymer is the sum of individual contributions.

Summary of Rouse model

- relaxation time of mode $p \sim \frac{1}{p^2}$
- $D_{\text{polymer}} \sim \frac{1}{N}$

Expt's of DNA in free soln.

$$\text{show } D \sim \frac{1}{N^{0.6}}$$

$$\tau_p \propto \frac{1}{p^2}$$

Rouse model fails of polymers in soln.
- neglects HI

When HI is not important in Expt's
(melt, confined DNA, narrow slit or channel)

Rouse model works

Dilute solns : need to account for
HI.

Sidetrack

Viscoelasticity



deformation is characterized by ΔL .

Shear stress

$$S = \frac{F}{A}$$

A = area that F acts on

Strain

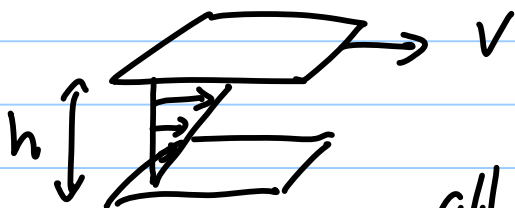
$$\gamma = \tan \alpha = \frac{\Delta L}{d}$$

- ① For ideal elastic solid, all mechanical energy is stored, no dissipation

$$S = G \cdot \gamma$$

G shear modulus

- ②. For ideal fluid



$$\dot{\gamma} = \frac{v}{h} = \frac{\partial v_x}{\partial y} = \text{shear rate}$$

all mechanical energy is dissipated by moving fluid

$$S = \frac{F_x}{A} = \eta \dot{\gamma}$$

η viscosity of fluid

Viscoelasticity : How "solid-like" or "fluid-like" is the material as a fcn. of time?

timescale \leftrightarrow "frequency" of probe

$$\omega = \frac{2\pi}{t}$$

Define instantaneous stress $S(t; \dot{\gamma})$

Define transient viscosity $\eta^\#(t, \dot{\gamma}) = \frac{S(t; \dot{\gamma})}{\dot{\gamma}}$

\Rightarrow info. about structure changes in complex fluid.

For "linear" viscoelastic regime, we can characterize the dynamic response by the "stress relaxation time" $G(t)$

memory of deformation.

$$S(t) = \int_{-\infty}^t G(t-t') \dot{\gamma}(t') dt'$$

\uparrow begin of expt.

$G(t-t') \equiv$ non-instantaneous rxn. of molecules due to external perturbation

Fluid: $G(t) \rightarrow 0$ $t \rightarrow \infty$

Solid: $G(t) \neq 0$ $t \rightarrow \infty$

e.g. (i) sudden application of strain (impulse)

$$\dot{\gamma}(t) = \gamma \delta(t) \quad \text{impulse @ } t=0.$$

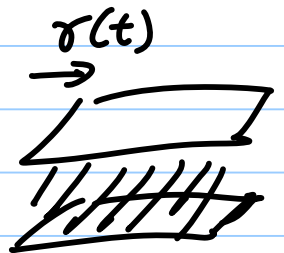
$$\Rightarrow S = \gamma G(t)$$

(ii) Oscillatory shear @ freq ω

dimensionless strain amplitude

$$= \gamma(t) = \gamma_0 \sin(\omega t)$$

\uparrow
max plate displacement



linear regime $\gamma_0 \ll 1$

stress can in-phase and out-of phase to oscillatory shear

$$S(t) \equiv \gamma_0 \left[G'(\omega) \sin(\omega t) + G''(\omega) \cos(\omega t) \right]$$

\uparrow
Storage modulus
(elastic)

\uparrow
loss modulus
(viscous)

G' & G'' carry the same info. as $G(t)$

can show $G''(\omega) = \omega \int_0^{\infty} dt \cos(\omega t) G(t)$

$$G'(\omega) = \omega \int_0^{\infty} dt \sin(\omega t) G(t)$$

shear viscosity $\eta = \lim_{t \rightarrow \infty} \frac{S(t)}{\dot{\gamma}(t)} \xrightarrow{\text{can show}} \lim_{\omega \rightarrow 0} \frac{G''(\omega)}{\omega}$

$$\lim_{\omega \rightarrow 0} \eta(\omega) \stackrel{\Downarrow}{=} \int_0^{\infty} dt G(t)$$

Example : "Maxwell fluid" (1867)

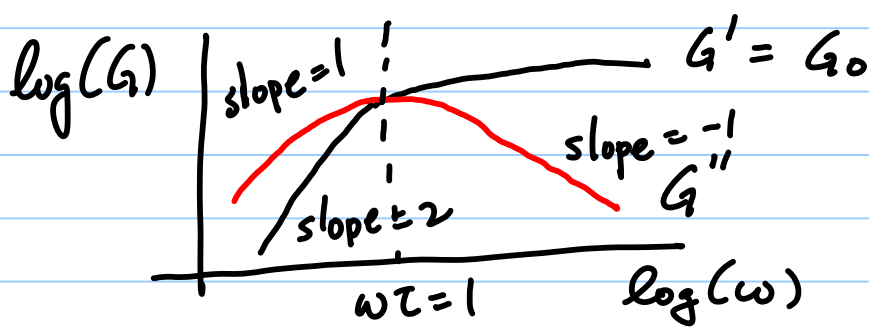
Simplest model of viscoelastic fluid

Only 1 relaxation time for stress relaxation

$$\Rightarrow G = G_0 e^{-t/\tau} \quad \tau \equiv \text{stress relax time.}$$

$$G'(\omega) = \omega \int_0^{\infty} dt \sin(\omega t) G(t) = G_0 \frac{(\omega\tau)^2}{1 + (\omega\tau)^2}$$

$$G''(\omega) = \omega \int_0^{\infty} dt \cos(\omega t) G(t) = G_0 \frac{(\omega\tau)}{1 + (\omega\tau)^2}$$



$$\eta = \lim_{\omega \rightarrow 0} \frac{1}{\omega} G''(\omega) = G_0 \tau \quad \leftarrow \text{Maxwell Egn.}$$

Small molecules : simple fluid , little complex structure

$$H_2O @ 25^\circ C \quad \eta = 10^{-2}$$

$$G_0 = 10^{11} \text{ Pa.}$$

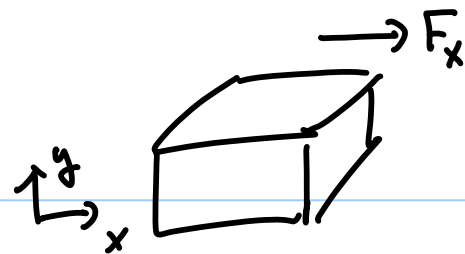
$$\tau \approx 10^{-15} \text{ s}$$

Complex fluid - polymers or dense colloids

much "softer"

G_0 much less
 τ much longer

Polymer stress relaxation



stress comes from chain connectivity.

Shear stress & total viscosity

$$\eta = \frac{\sigma_{x,y}}{\dot{\gamma}}$$

$$\underline{S} = \begin{bmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{bmatrix}$$

F_x on A_y

$$\eta = \eta_{\text{solvent}} + \int_0^{\infty} G(t) dt$$

2nd Green-Kubo Theorem

$$G(t) = \frac{1}{k_B T} \rho_p \langle J_{xy}(0) J_{xy}(t) \rangle$$

$$J_{xy}(t) = \sum_{\alpha=1}^N X_{\alpha}(t) F_{\alpha}^y(t)$$

\uparrow
x-displacement of segment α

\uparrow
y-component of spring force on segment α

$$\text{Rouse model} \Rightarrow F_{\alpha}^y(t) = -k_s [2y_{\alpha}(t) - y_{\alpha+1}(t) - y_{\alpha-1}(t)]$$

ideal coil

$$\Rightarrow k_s = \frac{3k_B T}{\sigma^2}$$

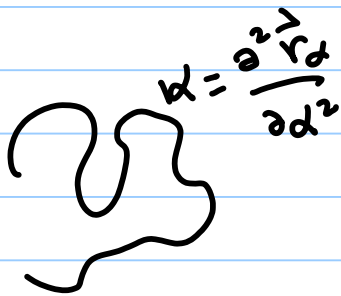
$$\approx -k_s \frac{\partial^2 y}{\partial \alpha^2}$$

$$\beta = \frac{1}{k_B T} \quad \frac{G(t)}{\rho \beta} = \sum_{\alpha=1}^N \sum_{\gamma=1}^N \langle X_{\alpha}(0) F_{\alpha}^y(0) X_{\gamma}(t) F_{\gamma}^y(t) \rangle$$

by linearity
& EOM

$$= \sum_{\alpha=1}^N \sum_{\gamma=1}^N \underbrace{\langle X_{\alpha}(0) X_{\gamma}(t) \rangle}_{\text{segmental displacement}} \underbrace{\langle F_{\alpha}^y(0) F_{\gamma}^y(t) \rangle}_{\text{dynamics of local curvature of chain backbone}}$$

Physically; $G(t)$ probes (i) segmental displacement



(ii) dynamics of local

Curvature of chain backbone

Switch to normal mode

$$Y_{\alpha}(t) = Y_0(t) + 2 \sum_{p=1}^{N-1} \cos\left(\frac{p\pi}{N} \alpha\right) Y_p(t)$$

$$\rightarrow Y_0(t) + 2 \int dp \cos\left(\frac{p\pi}{N} \alpha\right) Y_p(t)$$

$$\frac{F}{k_s} \sim \frac{\partial^2}{\partial \alpha^2} Y_{\alpha}(t) \Rightarrow -2 \int dp \left(\frac{p\pi}{N}\right)^2 \cos\left(\frac{p\pi}{N} \alpha\right) Y_p(t)$$

need $\langle X_p(t) X_{p'}(0) \rangle \neq \langle Y_p(t) Y_{p'}(0) \rangle \} \delta_{p,p'}$

Some manipulation

$$\Rightarrow G(t) \propto \frac{k_s^2 \beta \rho}{N^3} \sum_{p=1}^N p^4 C_{pp}^2(t)$$

$$C_{pp}(t) = \langle \vec{x}_p(0) \vec{x}_p(t) \rangle = \frac{3k_B T}{k_p} e^{-t/\tau_p}$$

$$= \frac{N \sigma^2}{2\pi^2} \frac{1}{p^2} e^{-t p^2 / \tau_R}$$

Classic
result

$$G(t) = \frac{k_B T}{N} \rho_{\text{seg}} \sum_{p=1}^N e^{-2t p^2 / \tau_R}$$

Short time : $G(t=0) = \rho_{\text{seg}} k_B T$

$$\tau_R = \frac{\rho_{\text{seg}} N b^2}{3\pi^2 k_B T}$$

Make 5 predictions

(i) short time ($t \ll \tau_R$)

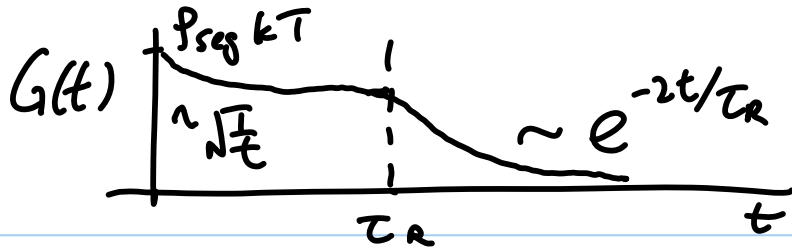
many modes to stress relaxation

$$\Rightarrow G(t) \propto \frac{k_B T}{N} \rho_{\text{seg}} \sqrt{\frac{\tau_R}{t}}$$

$$\propto \frac{1}{\sqrt{t}} \rho_{\text{seg}} \sqrt{k_B T \rho_{\text{seg}} b^2} \sim N^0$$

(ii) long time ($t > \tau_R$) $p=1$ dominate

$$G(t) \approx \frac{k_B T \rho_{\text{seg}}}{N} e^{-2t/\tau_R}$$



(iii) viscosity of polymer

$$\eta_{\text{poly}} = \int_0^{\infty} dt G_1(t) = \frac{p_{\text{seg}} k_B T}{N} \sum_{p=1}^N \frac{\tau_R}{2p^2}$$

dominant contribution from low $p \propto N p_{\text{seg}} \int b^2$.

(iv) COM diffusion : $D = \frac{k_B T}{N \zeta}$.

(v) oscillatory expt

$$G'(\omega) = \omega \int_0^{\infty} dt \sin(\omega t) G(t) \quad \tau_p = \frac{\tau_R}{2p^2}$$

$$= p_{\text{seg}} k_B T \sum_{p=1}^N \frac{(\omega \tau_p)^2}{1 + (\omega \tau_p)^2}$$

$$G''(\omega) = p_{\text{seg}} k_B T \sum_{p=1}^N \frac{(\omega \tau_p)}{1 + (\omega \tau_p)^2}$$

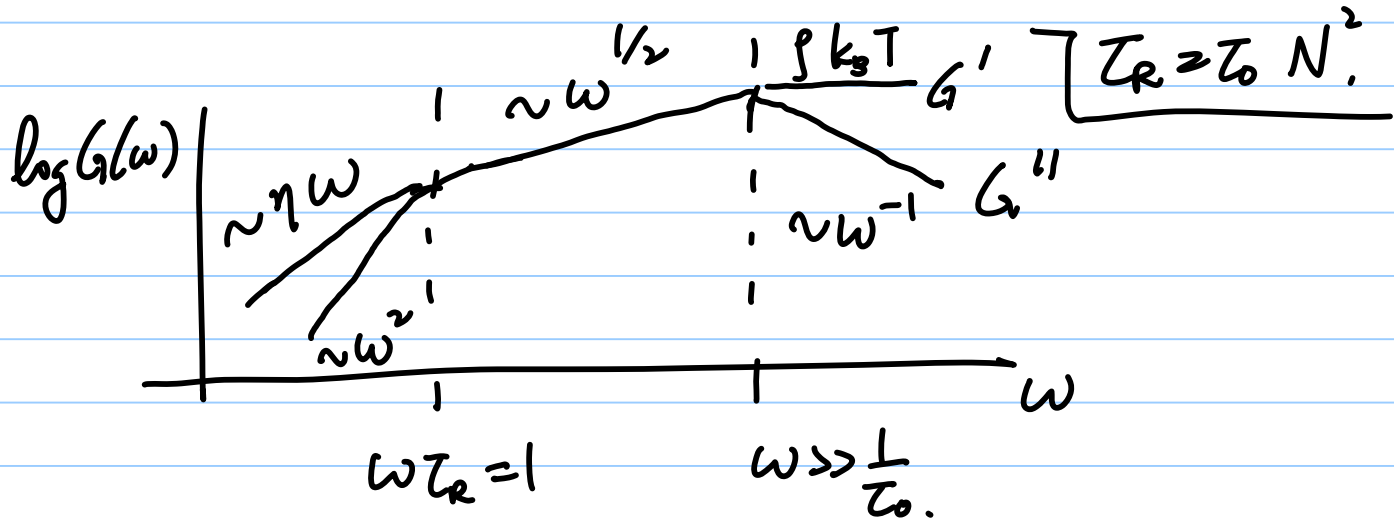
low ω , long time $G'(\omega) \propto (\omega \tau_R)^2$

$G''(\omega) \propto (\omega \tau_R)$

hi ω , short time $\Sigma \rightarrow \int dp$

$$G'(\omega) \sim G''(\omega) \propto \frac{1}{N} \sqrt{\omega \tau_R}$$

$$\propto \sqrt{\omega \tau_0}$$



Rouse
model

works for melt of short, unentangled chains.